



# Mode Transition Behavior in Hybrid Dynamic Systems

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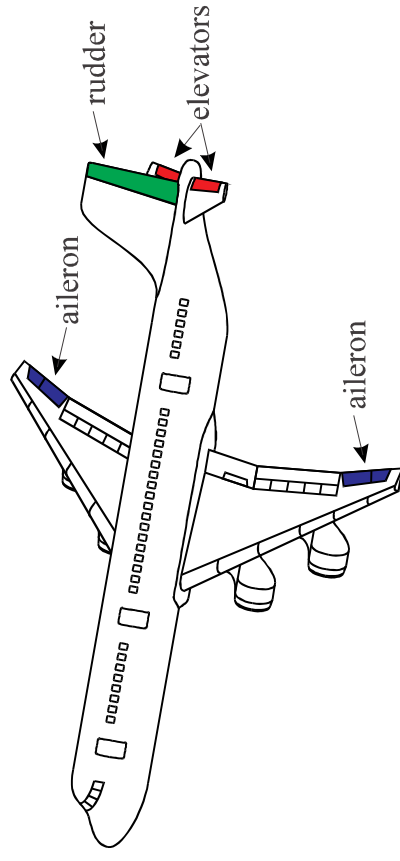


# Introduction

## Mode Transitions in Hybrid Models of Physical Systems

- ▶ hybrid because
  - continuous, differential equations
  - discrete, finite state machine
- ▶ overview of phenomena involved

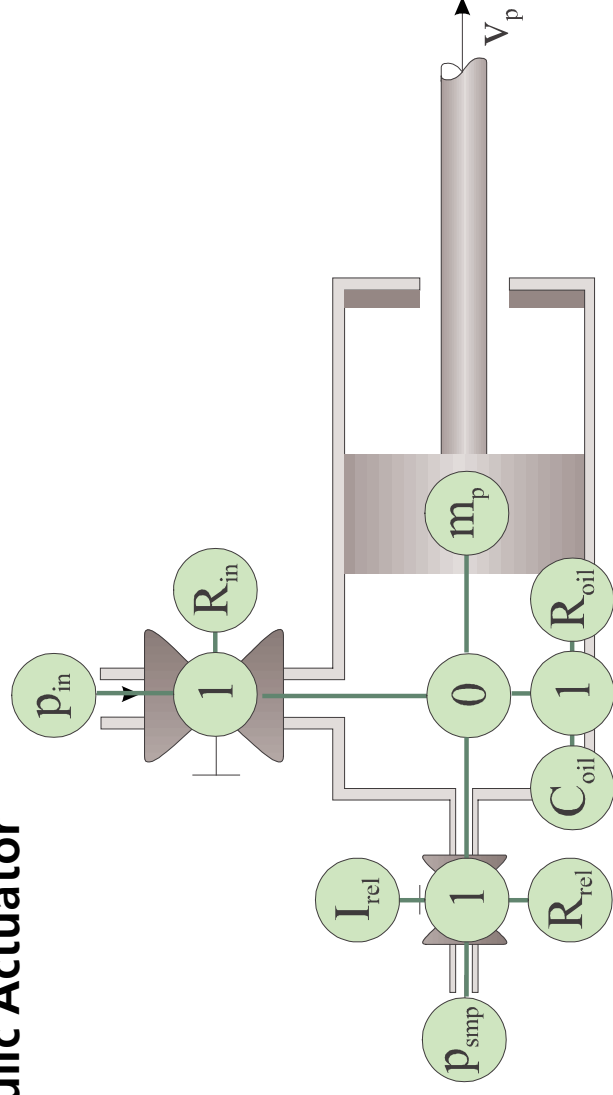
## Illustrated by Hydraulic Actuator Used for Aircraft Attitude Control Surfaces





# Modeling of Physical Systems

Ideal Picture Model (Schematic)  
 Identify Behavioral Phenomena  
 For Example, A Hydraulic Actuator





# Equation Generation

## Compile Constituent Equations

- $R_{in}$
- $R_{oil}$
- $C_{oil}$
- $m_p$
- $R_{rel}$
- $I_{rel}$
- 0, cylinder chamber
- 1, relief flow pipe
- 1, intake pipe
- 1, oil compression

$$f_{in}R_{in} = p_{Rin}$$

$$f_R R_{oil} = p_{Roil}$$

$$C_{oil} \dot{p}_C = f_R$$

$$m_p \dot{v}_p = A_p p_{cyl}$$

$$f_{rel} R_{rel} = p_{rel}$$

$$I_{rel} \dot{f}_{rel} = p_{rel}$$

$$v_p = f_{in} - f_{rel}$$

$$p_{rel} = p_{smp} - f_{rel} R_{rel} + p_{cyl}$$

$$p_{Rin} = p_{in} - p_{cyl}$$

$$p_{Roil} = p_{oil} - p_C$$



# Equation Processing

## Before Simulation

- ▶ the number of equations is reduced
  - substitution/elimination
- ▶ equations are sorted
  - each equation computes one variable
- ▶ equations are solved
  - high index problems may require differentiation of certain equations



# Hybrid Behavior

## Introduce Valves

- ▶ make highly nonlinear behavior piecewise linear
  - intake valve if  $v_{in}$  then  $p_{Rin} = p_{in} - p_{cyl}$  else  $f_{in} = 0$
  - relief valve if  $v_{rel}$  then  $p_{rel} = p_{smp} - f_{rel}R_{rel} + p_{cyl}$  else  $f_{rel} = 0$

## Switching Between Modes of Continuous Behavior

- ▶ intake valve,  $v_{in}$ , external switch (control law)
- ▶ relief valve,  $v_{rel}$ , autonomous switch triggered by physical quantities

$$v_{rel} = p_{cyl} > p_{th}$$

- ▶ different sets of equations



# Computational Causality

## When Switching Equations

- ▶ computational causality may change
  - re-ordering
  - re-solving

## Example

- ▶ when the intake valve closes, equations change
  - from  $p_{Rin} = p_{in} - p_{cyl}$
  - to  $f_{in} = 0$
- ▶ therefore, in this equation
  - $p_{Rin}$  becomes unknown
  - $f_{in}$  becomes known



# Implicit Modeling

Deal With Causal Changes Numerically

Valve Behavior

- ▶ residue on  $f_{in}$       $0 = \text{if } v_{in} \text{ then } -p_{Rin} + p_{in} - p_{cyl} \text{ else } f_{in}$
- ▶ residue on  $f_{rel}$       $0 = \text{if } v_{rel} \text{ then } -p_{rel} + p_{smp} - f_{rel}R_{rel} + p_{cyl} \text{ else } f_{rel}$

Implicit Numerical Solver (e.g., DASSL)

- ▶ designed to handle this formulation

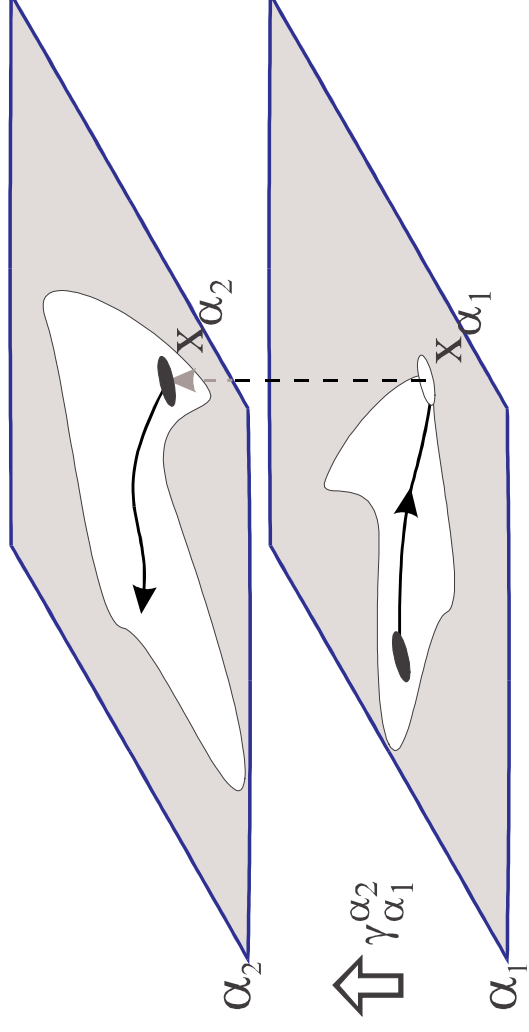




# Hybrid Dynamic Behavior

## Geometric View

- ▶ modes of continuous, smooth, behavior
- ▶ patches of admissible state variable values





# Specification Parts

## Hybrid Behavior Specification

- ▶ a function,  $f$ , that defines continuous, smooth, behavior for each mode
- ▶ an inequality,  $\gamma$ , that defines admissible state variable values

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i} u = 0$$

$$\gamma_{\alpha_i}^{\alpha_{i+1}}: C_{\alpha_i} x + D_{\alpha_i} u \geq 0$$



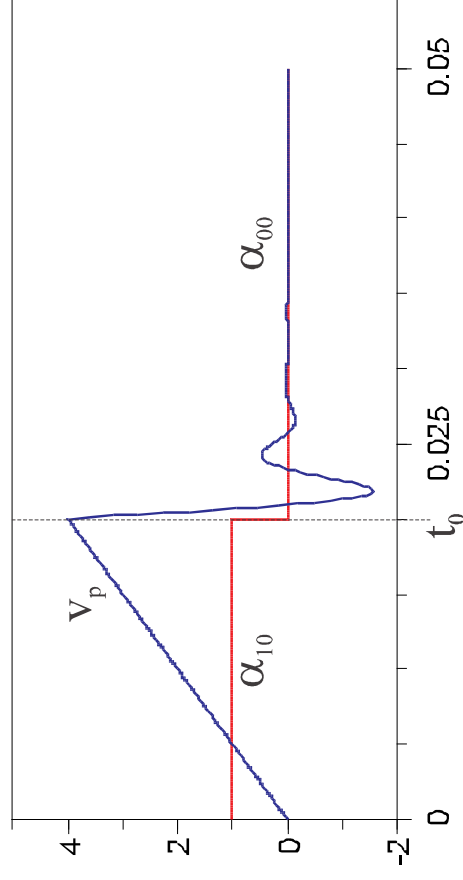
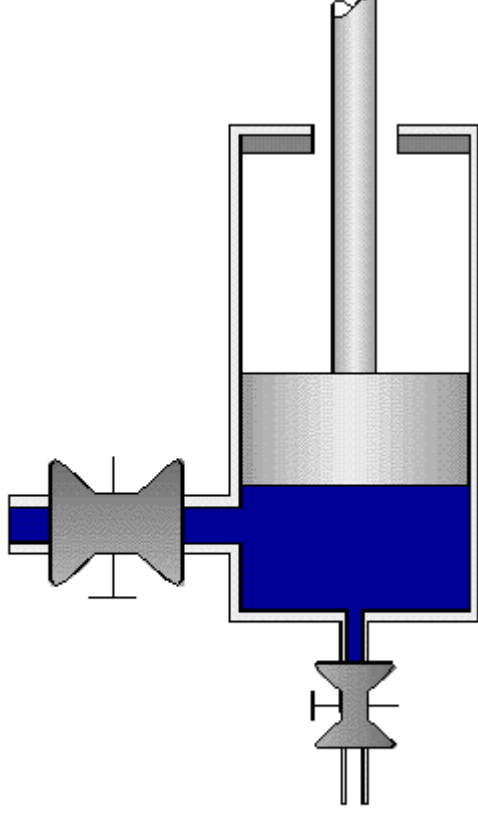
# Dynamics

## Behavior Characteristics

- ▶  $C^0$ , i.e., no jumps in state variables
- ▶ steep gradients

## Example

- ▶ when the intake valve closes, piston velocity quickly reduces to 0





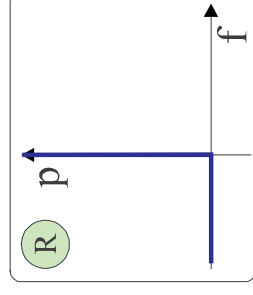
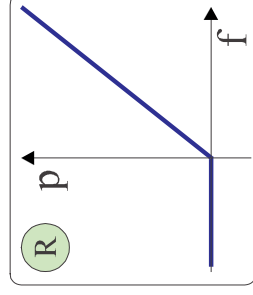
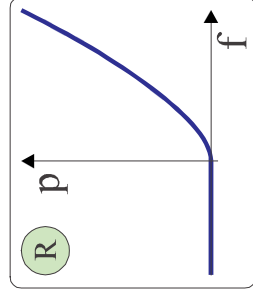
# The Next Step

## Remove Steep Gradients

- ▶ e.g., singular perturbation

## Algebraic Constraints Between State Variables

- ▶ high index systems
- ▶ subspace with admissible (continuous) dynamic behavior
- ▶ discontinuities (jumps) in state behavior

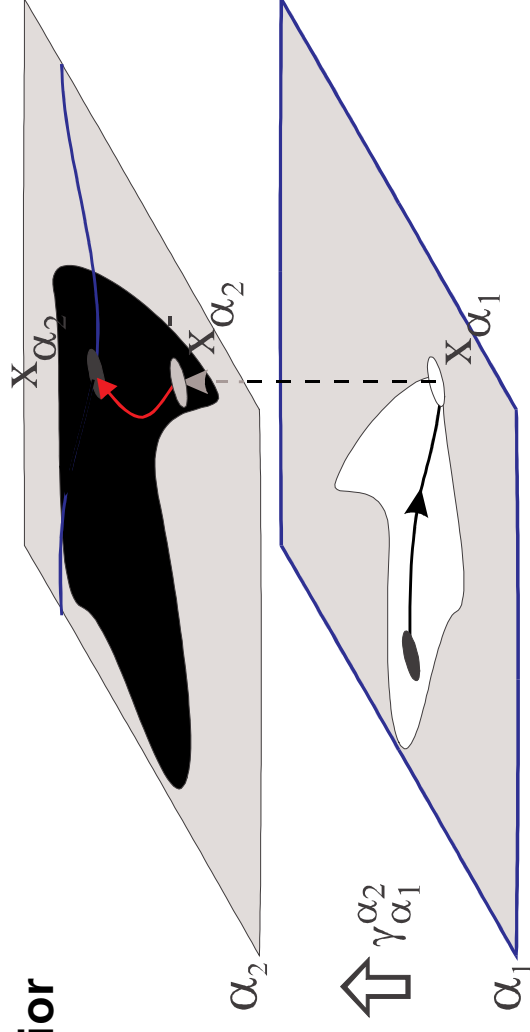




# Hybrid Dynamic Behavior - Refined

## Geometric View

- ▶ modes of continuous, smooth, behavior
- ▶ patches of admissible state variable values
- ▶ manifold of dynamic behavior





# Specification Parts

## Hybrid Behavior Specification

- ▶ a function,  $f$ , that implicitly defines for each mode
  - continuous, smooth, behavior
  - state variable value jumps
- ▶ an inequality,  $\gamma$ , that defines admissible generalized state variable values
- ▶ for explicit reinitialization (semantics of  $x^-$ )

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i} u = 0$$

$$\gamma_{\alpha_i}^{\alpha_{i+1}}: C_{\alpha_i} x + D_{\alpha_i} u \geq 0$$

$$f_{\alpha_i}: E_{\alpha_i} \dot{x} + A_{\alpha_i} x + B_{\alpha_i}^u u + B_{\alpha_i}^x x^- = 0$$



# Handling of Systems With High Index

## DASSL Handles Index 2 Systems

- ▶ implicit formulation for continuous behavior

## Requires Consistent Initial Conditions When Mode Changes Occur

- ▶ compute from implicit formulation to make jump space (projection) explicit
- ▶ for example, sequences of subspace iteration
  - space of dynamic behavior:  $V^{n+1} = A^{-1} E V^n$ ,  $V^0 = R^n$
  - jump space:  $T^{n+1} = E^{-1} A T^n$ ,  $T^0 = \{0\}$
- ▶ or, decomposition in (pseudo) Kronecker Normal Form



# Projections

## Linear Time Invariant Index 2 System

- ▶ derive pseudo Kronecker Normal Form (numerically stable)

$$\begin{bmatrix} E_{11} & 0 & 0 \\ 0 & 0 & E_{22,12} \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{x}_f \\ \dot{x}_{i,1} \\ \dot{x}_{i,2} \end{bmatrix} + \begin{bmatrix} A_{11} & A_{12,1} & A_{12,2} \\ 0 & A_{22,11} & A_{22,12} \\ 0 & 0 & A_{22,22} \end{bmatrix} \begin{bmatrix} x_f \\ x_{i,1} \\ x_{i,2} \end{bmatrix} + \begin{bmatrix} B_1 \\ B_{2,1} \\ B_{2,2} \end{bmatrix} u = 0$$

- ▶ after integration (no impulsive input behavior), consistent values are

$$x_f = \bar{x}_f - E_{11}^{-1} A_{12,1} A_{22,11}^{-1} E_{22,12} (x_{i,2} - \bar{x}_{i,2})$$

$$x_{i,1} = A_{22,11}^{-1} (-B_{2,1} u + E_{22,12} \dot{x}_{i,2}) - A_{22,12} x_{i,2}$$

$$x_{i,2} = -A_{22,22}^{-1} B_{2,2} u$$





# The Hydraulic Actuator

## Generalized State Jumps for Each Mode

| Mode          | Projection                                                                                                                 |
|---------------|----------------------------------------------------------------------------------------------------------------------------|
| $\alpha_{00}$ | $f_{rel} = 0$<br>$v_p = 0$                                                                                                 |
| $\alpha_{01}$ | $v_p = (m_p v_p^- - I_{rel} f_{rel}^-) / (m_{rel} + m_p)$<br>$f_{rel} = (m_p v_p^- - I_{rel} f_{rel}^-) / (m_{rel} + m_p)$ |
| $\alpha_{10}$ | $v_p = v_p^-$<br>$f_{rel} = 0$                                                                                             |
| $\alpha_{11}$ | $v_p = v_p^-$<br>$f_{rel} = f_{rel}^-$                                                                                     |



## A Scenario

**Intake Valve Is Open**

- ▶ piston starts to move

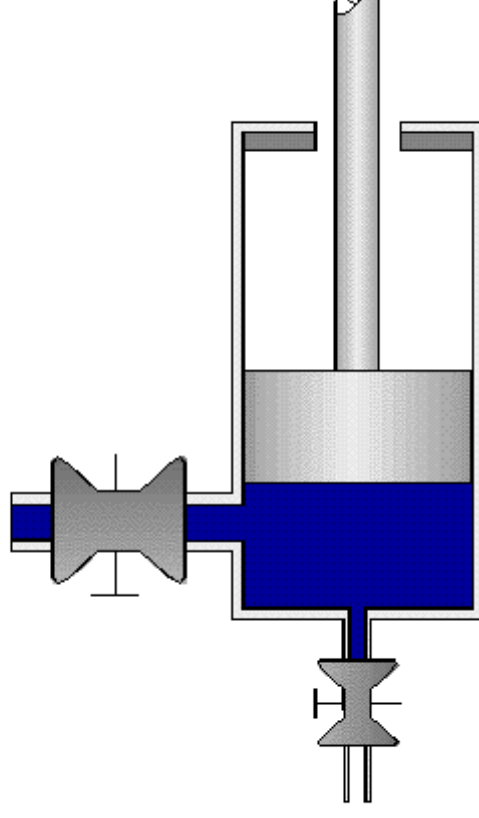
**Intake Valve Closes**

- ▶ piston inertia causes pressure build-up
- ▶ pressure reaches critical value

**Relief Valve Opens**

- ▶ cylinder pressure decreases

⇒ **Interaction Between Mode Transition Behavior**

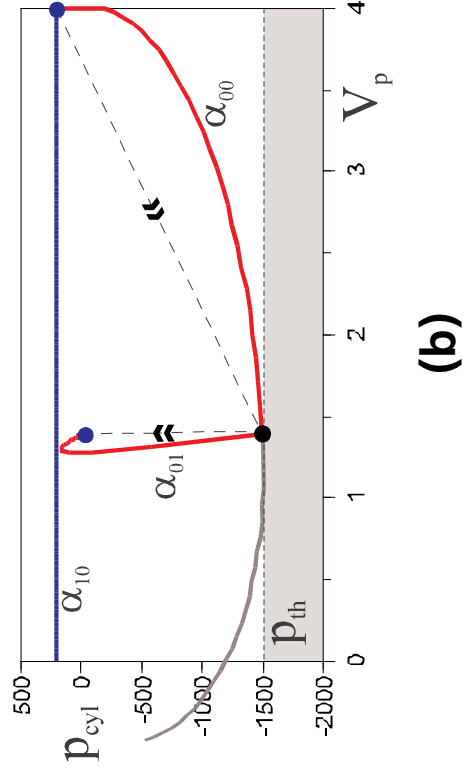
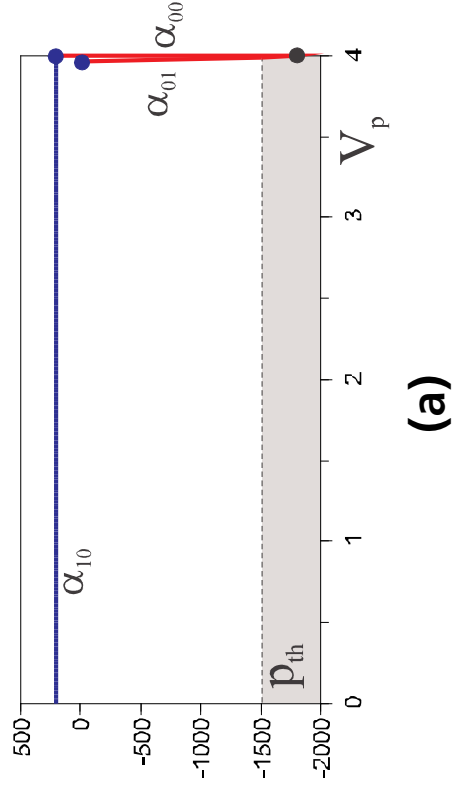




# Phase Space of Cylinder Scenario

## Projection Is Aborted

- ▶ immediately
- ▶ after partial completion

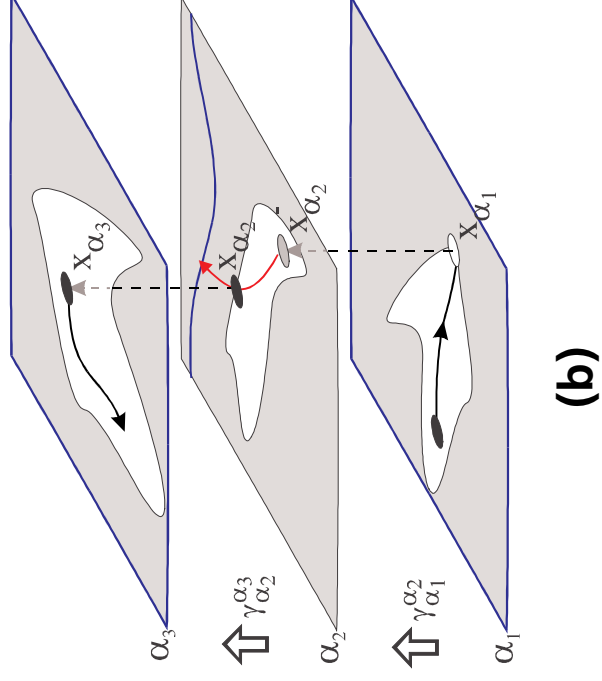
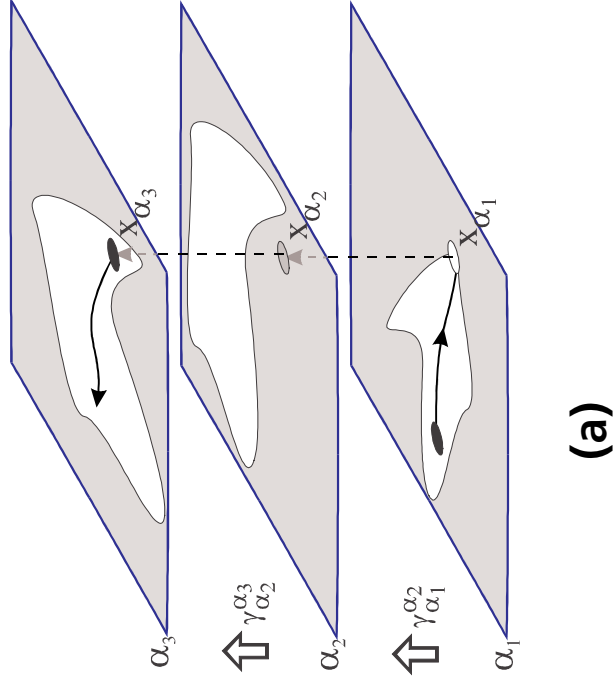




# Sequences of Mode Changes

(a) State Outside of a Patch in the New Mode

(b) During Projection State Values are Reached Outside of a Patch in the New Mode





# Impulses

## High Index Systems May Contain Impulsive Behavior

- ▶ in case of the hydraulic cylinder,  $p > p_{thr}$  would always hold if not  $v_p = v_p^-$
- ▶ unknown where the patch is abandoned

## In-Depth Analysis of Switching Conditions

- ▶ solve for required  $x(t)$
- ▶ compute earliest  $t = t_s$  at which  $\gamma(x(t), u(t), t) \geq 0$
- ▶ substitute  $t_s$  to compute  $x(t_s)$

## Complex Switching Structure

## Additional Difficulty When Interacting Fast Transients (e.g., collision)



## Detailed Analysis of the Projection

Cylinder Example (Imaginary Eigenvalues,  $\lambda = \lambda_r + i \lambda_i$ )

► from detailed model

- solve for  $p$

$$p(t) = e^{\lambda_r t} \left( p^- \cos(\lambda_i t) - \frac{1}{\lambda_i} \left( \frac{1}{C_1} v_p^- + \lambda_r p^- \right) \sin(\lambda_i t) \right)$$

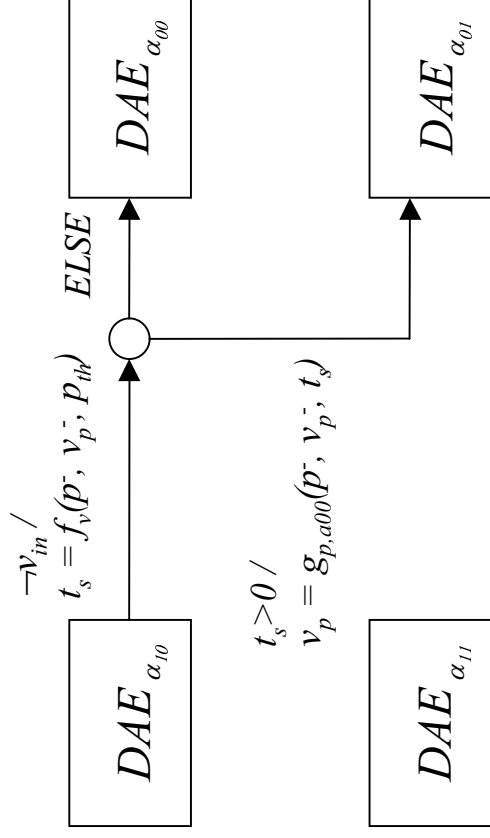
- substitute  $t$  at which  $p(t) > p_{th}$

$$v_p = e^{\lambda_r t_s} \left( v_p^- \cos(\lambda_i t) - \left( \frac{R_2}{I_1} v_p^- - \frac{p_1}{I_1} + \lambda_r v_p^- \right) \frac{\sin(\lambda_i t_s)}{\lambda_i} \right)$$



# Complex Switching Structure

## Explicit Re-Initialization

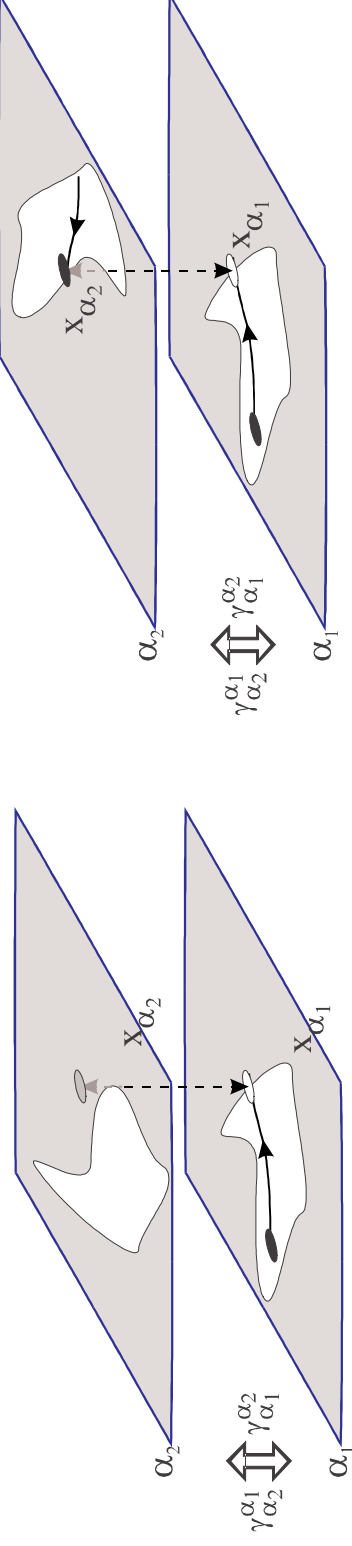




# Chattering

## What If the New Mode Switches Back

- ▶ immediately  $\Rightarrow$  inconsistent model, no solution
- ▶ after infinitesimal period of time  $\Rightarrow$  chattering behavior, solve with
  - equivalent control
  - equivalent dynamics



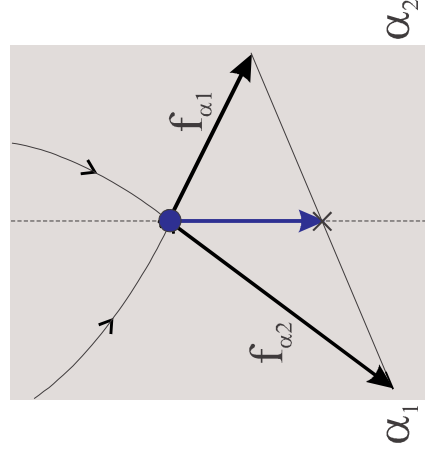




# Equivalent Dynamics

## Chattering

- ▶ fast component
  - remove
- ▶ slow component
  - weighted mean of instantaneous vector fields (Filippov Construction)
- ▶ sliding behavior





# Ontology

## Phase Space Transition Behavior Classification

- ▶ mythical (state invariant)
- ▶ pinnacle (state projection aborted)
- ▶ continuous
  - interior (continuous behavior)
  - boundary (further transition after infinitesimal time advance)
  - sliding (repeated transitions after each infinitesimal time advance)

## Combinations of Behavior Classes



# Conclusions

## Mode Transition Behavior

- ▶ Rich
- ▶ Complex

## Requires

- ▶ special algorithms/computations
- ▶ model verification analyses

**How to Efficiently Generate Behavior (e.g., for Real-time Applications)?**